# I.N.G. FIXATIONS



# **ÉVALUATION TECHNIQUE EUROPÉENNE**



ETE - 25/0338

# RAPIDO® M6 Piton de suspension direct béton



ETA-Danmark A/S Göteborg Plads 1 DK-2150 Nordhavn Tel. +45 72 24 59 00 Internet www.etadanmark.dk Authorised and notified according to Article 29 of the Regulation (EU) No 305/2011 of the European Parliament and of the Council of 9 March 2011



# European Technical Assessment ETA-25/0338 of 2025/06/20

I General Part

**Technical Assessment Body issuing the ETA and designated according to Article 29 of the Regulation (EU) No 305/2011:** ETA-Danmark A/S

Trade name of the Rapido construction product: **Product family to which** Concrete screw for use in concrete for redundant nonthe above construction structural systems product belongs: Manufacturer: **ING** Fixations Z. I. de Chassende BP 90168 F-43005 Le Puy-En-Velay Cedex France Manufacturing plant: **ING** Fixations Z. I. Chavanon F-43120 Monistrol-sur-Loire France This European Technical 15 pages including 9 annexes which form an integral Assessment contains: part of the document This European Technical Assessment is issued in EAD 330232-01-0601; Mechanical fasteners for use in accordance with concrete **Regulation (EU) No** 305/2011, on the basis of: This version replaces:

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### II SPECIFIC PART OF THE EUROPEAN TECHNICAL ASSESSMENT

#### **1** Technical description of product

The Rapido concrete screw is a screw fastener of size 6 for use in concrete for redundant non-structural systems. It has a nominal embedment depth of  $h_{nom}=35$  mm and the fastener shall only be used in dry internal conditions.

The Rapido concrete screw consists of steel with a zinc plated coating and the following steel characteristics:  $f_{uk}$ =400 MPa;  $f_{yk}$ =320 MPa.

The fastener is suitable for use in both cracked and uncracked concrete of strength classes C20/25 to C50/60.

The product description is given in Annex A and the intended use specifications of the product are detailed in Annex B.

#### 2 Specification of the intended use(s) in accordance with the applicable European Assessment Document (hereinafter EAD)

The performances given in Section 3 are only valid if the anchor is used in compliance with the specifications and conditions given in Annex B.

The provisions made in this European Technical Assessment are based on an assumed intended working life of the anchor of 50 years.

The indications given on the working life cannot be interpreted as a guarantee given by the producer or Assessment Body, but are to be regarded only as a means for choosing the right products in relation to the expected economically reasonable working life of the works.

# **3** Performance of the product and references to the methods used for its assessment

Characteristic

#### Assessment of characteristic

3.1 Mechanical resistance and stability (BWR1)

#### Characteristic resistance to tension load (static and quasi-static loading) Method A

Resistance to steel failure	Annex C
Resistance to pull-out failure	Annex C
Resistance to concrete cone failure	Annex C
Robustness	Annex C
Minimum edge distance and spacing	Annex C
Edge distance to prevent splitting under load	Annex C
Characteristic resistance to shear load (static a	nd quasi-static loading)
Resistance to steel failure under shear load	Annex C
Resistance to pry-out failure	Annex C
Characteristic resistance for simplified design	
Method B	Not relevant
Method C	Not relevant
Displacements	
Displacements under static and quasi-static loading	No performance assessed
Characteristic resistance and displacements for	seismic performance categories C1 and C2
Resistance to tension load, displacements	No performance assessed
Resistance to shear load, displacements	No performance assessed
Factor for annual gap	No performance assessed
3.2 Safety in case of fire (BWR2)	
Reaction to fire	The fastener is made from steel classified as performance Class A1 of the characteristic reaction to fire, in accordance with the provisions of EC decision 96/603/EC, amended by EC Decision 2000/605/EC.

### Characteristic Assessment of characteristic

#### **Resistance to fire**

Fire resistance to steel failure (tension load)	Annex C
Fire resistance to pull-out failure (tension load)	Annex C
Fire resistance to steel failure (shear load)	Annex C
<b>3.3</b> Aspects of durability	
Durability	Annex B

See additional information in section 3.9

# **3.9** General aspects related to the performance of the product

The European Technical Assessment is issued for the product on the basis of agreed data/information, deposited with ETA-Danmark, which identifies the product that has been assessed and judged. Changes to the product or production process, which could result in this deposited data/information being incorrect, should be notified to ETA-Danmark before the changes are introduced. ETA-Danmark will decide whether or not such changes affect the ETA and consequently the validity of the CE marking on the basis of the ETA and if so whether further assessment or alterations to the ETA, shall be necessary.

## 4 Assessment and verification of constancy of performance (AVCP) (hereinafter AVCP) system applied, with reference to its legal base

#### 4.1 AVCP system

According to the decision 1996/582/EC of the European Commission, the system(s) of assessment and verification of constancy of performance (see Annex V to Regulation (EU) No. 305/2011) is 1.

# 5 Technical details necessary for the implementation of the AVCP system, as provided for in the applicable EAD

Technical details necessary for the implementation of the AVCP system are laid down in the control plan deposited at ETA-Danmark prior to CE marking

Issued in Copenhagen on 2025-06-20 by

Thomas Bruun Managing Director, ETA-Danmark





## **Specifications**

#### Anchor subject to:

- Static and quasi static loads
- For use in redundant non-structural systems
- Anchorages with requirements related to resistance to fire

#### Base materials:

- Compacted reinforced and compacted unreinforced concrete without fibers according to EN 206:2013.
- Strength classes C20/25 to C50/60 according to EN 206:2013.
- Cracked or uncracked concrete.

#### Use conditions:

• Anchorages subjected to dry internal exposure conditions.

#### Design:

- Anchorages are designed under the responsibility of an engineer experienced in anchorages and concrete work.
- Verifiable calculation rules and drawings are prepared taking into account of the loads to be anchored. The position of the fastener is indicated on the design drawings (e.g., position of the fastener relative to reinforcement or to supports, etc.).
- Anchorages under static or quasi static actions and under fire exposure are designed in accordance with EN 1992-4:2018.

#### Installation:

- Hammer drilling only
- Anchor installation carried out by appropriately qualified personal and under the supervision of the person responsible for technical matters of the site.
- In case of aborted hole: new drilling at a minimum distance away of twice the depth of aborted hole or smaller distance if the aborted hole is filled with high strength mortar and if under shear or oblique tension load it is not the direction of the load application.
- After installation further turning of the anchor must not be possible.
- The head of the fastener must be in contact with the substrate and is not damaged.

#### RAPIDO Concrete screw

Annex B1

Intented use Specifications of European Technical Assessment ETA-25/0338

# Installation parameters

Rapido concrete screw			
Nominal anchorage depth	h <sub>nom</sub>	[mm]	35
Nominal drill hole diameter	do	[mm]	6
Cutting diameter of drill bit	d <sub>cut</sub> ≤	[mm]	6,4
Drill hole depth	h₁≥	[mm]	40
Installation torque <sup>1)</sup>	T <sub>inst</sub> ≥	[Nm]	3
instantion torque	T <sub>inst, max</sub> ≤	[Nm]	9

<sup>1)</sup> Apply the minimum torque required to set the fastener till the head is in contact with concrete surface.



- $h_{nom}$  = nominal anchorage depth
- h<sub>min</sub> = minimum thickness of member

## Annex B2

of European Technical Assessment ETA-25/0338

Installation parameters

# Minimum thickness of member, minimum spacing and edge distance

Rapido concrete screw			
Minimum thickness of member	h <sub>min</sub>	[mm]	80
Minimum edge distance	C <sub>min</sub>	[mm]	150
Minimum spacing	Smin	[mm]	150



#### **RAPIDO Concrete screw**

#### Intented use

Minimum thickness of member, minimum spacing and edge distance

of European Technical Assessment ETA-25/0338

Annex B3

Installation instruction	ons	
	Drill a hole with hammer drilling machine with nomin required depth 40 mm.	nal drill Ø 6 mm to the
	Remove drill dust by vacuuming or blowing of.	
3	Install with rotary screwdriver or torque wrench ( <b>no</b> Apply the minimum torque required to set the faster with concrete surface.	
4 4 The use of impact screwdrive Apply the minimum torque re	Rapido is installed. er is not allowed. equired to set the fastener till the head is in contac	t with concrete surface.
		Annex B4
RAPIDO Concrete screw		of European
Intented use Installation instructions		Technical Assessment ETA-25/0338

# Characteristic values for static and quasi-static loading

Rapido concret	e screw			6
Nominal embed	lment depth h	nom	[mm]	35
Steel failure for	tension an sl	near loadin	g	
Characteristic te	ension load	N <sub>Rk,s</sub>	[kN]	9,9
Partial factor		¥мs,n	[-]	1,5
Characteristic s	hear load	V <sub>Rk,s</sub>	[kN]	6,8
Partial factor		¥ms,∨	[-]	1,25
Ductility factor <sup>1)</sup>		<b>k</b> 7	[-]	-
Characteristic b	ending load	M <sup>0</sup> <sub>Rk,s</sub>	[Nm]	8,3
Pull-out failure	1	1		
Characteristic	cracked	N <sub>Rk,p</sub>	[kN]	0,9
tension load C20/25	uncracked	N <sub>Rk,p</sub>	[kN]	1,5
Increasing	C30/37			1,22
factor Ψ <sub>c</sub> for N <sub>Rk,p</sub> =	C40/50	Ψ <sub>c</sub>	[-]	1,41
$N_{Rk,p(C20/25)}^*\Psi_c$	C50/60			1,58
Concrete failure	. Splitting fai		oto cono failura	and pry-out failure
Effective embed		h <sub>ef</sub>	[mm]	22,4
	cracked	k <sub>cr</sub>	[-]	7,7
k-factor	uncracked	K <sub>cr</sub> K <sub>ucr</sub>	[-]	11,0
Concrete				3 x h <sub>ef</sub>
cone failure	spacing edge	S <sub>cr,N</sub>	[mm] [mm]	J X Hef
	distance	C <sub>cr,N</sub>	[11111]	1,5 x h <sub>ef</sub>

	distance	,		,
	spacing	S <sub>cr,sp</sub>	[mm]	300
	edge distance	C <sub>cr,sp</sub>	[mm]	150
Factor for pry-o	ut failure	k <sub>8</sub>	[-]	1,0
Installation factor	or	γinst	[-]	1,2

Concrete edge failure			
Effective length in concrete	l <sub>f</sub> = h <sub>ef</sub>	[mm]	22,4
Nominal outer diameter of screw	d <sub>nom</sub>	[mm]	6

 $^{1)}\,$  the socket head fastener is installed directly in the concrete without a base steel plate, therefore factor  $k_7$  to account for the ductility of the fastener for group of fasteners is not given.

#### **RAPIDO Concrete screw**

#### Performances

Characteristic values for static and quasi-static loading

of European Technical Assessment ETA-25/0338

Annex C1

# Fire exposure - characteristic values of resistance

Optional fire tests were not performed, therefore the fire resistance for normal weight concrete C20/25 to C50/60 is calculated.

Characteristic values for tension loading under fire exposure - normal weight concrete

	Size		6
	h <sub>nom</sub> (mm)		35
Steel failu	ire		
R30	N <sub>Rk,s,fi</sub>	(kN)	0,25
R60	N <sub>Rk,s,fi</sub>	(kN)	0,22
R90	N <sub>Rk,s,fi</sub>	(kN)	0,17
R120	N <sub>Rk,s,fi</sub>	(kN)	0,12
Pullout fa	ilure		
R30	N <sub>Rk,p,fi</sub>	(kN)	
R60	N <sub>Rk,p,fi</sub>	(kN)	0,23
R90	N <sub>Rk,p,fi</sub>	(kN)	
R120	N <sub>Rk,p,fi</sub>	(kN)	0,18
Concrete	cone failure	Ð	
R30	N <sub>Rk,c,fi</sub>	(kN)	
R60	N <sub>Rk,c,fi</sub>	(kN)	0,41
R90	N <sub>Rk,c,fi</sub>	(kN)	
R120	N <sub>Rk,c,fi</sub>	(kN)	0,33
Spacing			
	S <sub>cr,N</sub>	mm	4*hef
Edge dist	ance		L
	C <sub>cr,n</sub>	mm	2*hef
	- C <sub>min</sub>	mm	Fire attack from one side: 2hef
			Fire attack from more than one side: max (300;2hef)

RAPIDO Concrete screw

#### Performances

Fire exposure - characteristic values of tension resistance

of European Technical Assessment ETA-25/0338

Annex C2

ETA-20/0330

# Fire exposure - characteristic values of resistance

Optional fire tests were not performed, therefore the fire resistance for normal weight concrete C20/25 to C50/60 is calculated.

Characteristic values for shear loading under fire exposure - normal weight concrete

R30 $V_{Rk,s,fi}$ (kN)       0,25         R60 $V_{Rk,s,fi}$ (kN)       0,12         R90 $V_{Rk,s,fi}$ (kN)       0,17         R120 $V_{Rk,s,fi}$ (kN)       0,12         Steel failure with lever arm         R30 $M^0_{Rk,s,fi}$ (kN)       0,21         R60 $M^0_{Rk,s,fi}$ (kN)       0,19         R90 $M^0_{Rk,s,fi}$ (kN)       0,14         R120 $M^0_{Rk,s,fi}$ (kN)       0,10         Pryout Failure $R30$ $V_{Rk,cp,fi}$ (kN)         R60 $V_{Rk,cp,fi}$ (kN)       0,41         R90 $V_{Rk,cp,fi}$ (kN)       0,41         R90 $V_{Rk,cp,fi}$ (kN)       0,33         Concrete Edge Failure         The initial value Vork,cfi of the characteristic resistance in concrete C20/25 to C50/60 under fire exposure may be determined by:         Vork,c.fi = 0,25 x Vork,c (< R90)         Vork,c.fi = 0,20 x Vork,c (< R120)	Steel failu			6		
R60         V <sub>Rk,s,fi</sub> (kN)         0,22           R90         V <sub>Rk,s,fi</sub> (kN)         0,17           R120         V <sub>Rk,s,fi</sub> (kN)         0,12           Steel failure with lever arm           R30         M <sup>0</sup> <sub>Rk,s,fi</sub> (kN)         0,21           R60         M <sup>0</sup> <sub>Rk,s,fi</sub> (kN)         0,19           R90         M <sup>0</sup> <sub>Rk,s,fi</sub> (kN)         0,14           R120         M <sup>0</sup> <sub>Rk,s,fi</sub> (kN)         0,10           Pryout Failure         0,10         0,41         0,41           R90         V <sub>Rk,cp,fi</sub> (kN)         0,33           Concrete Edge Failure         0,33         Concrete Edge Failure           The initial value Vork,c <sub>fi</sub> of the characteristic resistance in concrete C20/25 to C50/60 under fire exposure may be determined by:         Vork,c <sub>fi</sub> = 0,20 x Vork,c (< R120)	Steel failu	h <sub>nom</sub> (mm)		35		
R60 $V_{Rk,s,fi}$ $(kN)$ $0,22$ R90 $V_{Rk,s,fi}$ $(kN)$ $0,17$ R120 $V_{Rk,s,fi}$ $(kN)$ $0,12$ Steel failure with lever arm           R30 $M^0_{Rk,s,fi}$ $(kN)$ $0,21$ R60 $M^0_{Rk,s,fi}$ $(kN)$ $0,19$ R90 $M^0_{Rk,s,fi}$ $(kN)$ $0,14$ R120 $M^0_{Rk,s,fi}$ $(kN)$ $0,10$ Pryout Failure           R30 $V_{Rk,cp,fi}$ $(kN)$ R60 $V_{Rk,cp,fi}$ $(kN)$ R60 $V_{Rk,cp,fi}$ $(kN)$ R120 $V_{Rk,cp,fi}$ $(kN)$ R120 $V_{Rk,cp,fi}$ $(kN)$ R120 $V_{Rk,cfi}$ $0,33$ Concrete Edge Failure           The initial value Vork,cfi of the characteristic resistance in concrete C20/25 to C50/60 under fire exposure may be determined by:           Vork,c,fi = $0,25 \times V$ ork,c ( $\leq R90$ ) $V$ ork,c,fi = $0,20 \times V$ ork,c ( $\leq R120$ )		ire without l	ever arm			
R90 $V_{Rk,s,fi}$ (kN)         0,17           R120 $V_{Rk,s,fi}$ (kN)         0,12           Steel failure with lever arm           R30 $M^0_{Rk,s,fi}$ (kN)         0,21           R60 $M^0_{Rk,s,fi}$ (kN)         0,19           R90 $M^0_{Rk,s,fi}$ (kN)         0,14           R120 $M^0_{Rk,s,fi}$ (kN)         0,10           Pryout Failure           R30 $V_{Rk,cp,fi}$ (kN)         0,41           R90 $V_{Rk,cp,fi}$ (kN)         0,41           R90 $V_{Rk,cp,fi}$ (kN)         0,33           Concrete Edge Failure         0,33         Concrete Edge Failure         The initial value Vork,c,fi of the characteristic resistance in concrete C20/25 to C50/60 under fire exposure may be determined by:         Vork,c,fi = 0,25 x Vork,c (< R90)         Vork,c,fi = 0,20 x Vork,c (< R120)	R30	V <sub>Rk,s,fi</sub>	(kN)	0,25		
R120 $V_{Rk,s,fi}$ (kN)         0,12           Steel failure with lever arm           R30 $M^0_{Rk,s,fi}$ (kN)         0,21           R60 $M^0_{Rk,s,fi}$ (kN)         0,19           R90 $M^0_{Rk,s,fi}$ (kN)         0,14           R120 $M^0_{Rk,s,fi}$ (kN)         0,10           Pryout Failure         R30 $V_{Rk,cp,fi}$ (kN)         0,41           R90 $V_{Rk,cp,fi}$ (kN)         0,41           R90 $V_{Rk,cp,fi}$ (kN)         0,33           Concrete Edge Failure         The initial value Vork,c,fi of the characteristic resistance in concrete C20/25 to C50/60 under fire exposure may be determined by:	R60	$V_{Rk,s,fi}$	(kN)	0,22		
Steel failure with lever armR30 $M^0_{Rk,s,fi}$ (kN)0,21R60 $M^0_{Rk,s,fi}$ (kN)0,19R90 $M^0_{Rk,s,fi}$ (kN)0,14R120 $M^0_{Rk,s,fi}$ (kN)0,10Pryout FailureR30 $V_{Rk,cp,fi}$ (kN)R60 $V_{Rk,cp,fi}$ (kN)R120 $V_{Rk,cp,fi}$ (kN)R120 $V_{Rk,cp,fi}$ (kN)R120 $V_{Rk,cp,fi}$ (kN)0,33Concrete Edge FailureThe initial value VORK,c,fi of the characteristic resistance in concrete C20/25 to C50/60under fire exposure may be determined by:VORK,c,fi = 0,25 x VORK,c (≤ R90)VORK,c,fi = 0,20 x VORK,c (≤ R120)With Vork,c initial value of the characteristic resistance in cracked concrete C20/25 under	R90	V <sub>Rk,s,fi</sub>	(kN)	0,17		
$ \begin{array}{ c c c c c } \hline R30 & M^0_{Rk,s,fi} & (kN) & 0,21 \\ \hline R60 & M^0_{Rk,s,fi} & (kN) & 0,19 \\ \hline R90 & M^0_{Rk,s,fi} & (kN) & 0,14 \\ \hline R120 & M^0_{Rk,s,fi} & (kN) & 0,10 \\ \hline \hline Pryout Failure \\ \hline \hline R30 & V_{Rk,cp,fi} & (kN) & 0,41 \\ \hline R60 & V_{Rk,cp,fi} & (kN) & 0,41 \\ \hline R90 & V_{Rk,cp,fi} & (kN) & 0,33 \\ \hline \hline R120 & V_{Rk,cp,fi} & (kN) & 0,33 \\ \hline \hline$	R120	V <sub>Rk,s,fi</sub>	(kN)	0,12		
R60 $M^0_{Rk,s,fi}$ $(kN)$ $0,19$ R90 $M^0_{Rk,s,fi}$ $(kN)$ $0,14$ R120 $M^0_{Rk,s,fi}$ $(kN)$ $0,10$ Pryout FailureR30 $V_{Rk,cp,fi}$ $(kN)$ $0,41$ R90 $V_{Rk,cp,fi}$ $(kN)$ $0,41$ R90 $V_{Rk,cp,fi}$ $(kN)$ $0,33$ Concrete Edge Failure $0,33$ $0,33$ The initial value Vork,c,fi of the characteristic resistance in concrete C20/25 to C50/60 under fire exposure may be determined by:Vork,c,fi = $0,25 \times Vork,c$ ( $\leq R90$ )Vork,c,fi = $0,20 \times Vork,c$ ( $\leq R120$ )With Vork,c initial value of the characteristic resistance in cracked concrete C20/25 under	Steel failu	ire with leve	er arm			
$\begin{array}{c c c c c c c } \hline R90 & M^0_{Rk,s,fi} & (kN) & 0,14 \\ \hline R120 & M^0_{Rk,s,fi} & (kN) & 0,10 \\ \hline Pryout Failure \\ \hline \hline R30 & V_{Rk,cp,fi} & (kN) & \\ \hline R60 & V_{Rk,cp,fi} & (kN) & \\ \hline R90 & V_{Rk,cp,fi} & (kN) & \\ \hline R120 & V_{Rk,cp,fi} & (kN) & 0,33 \\ \hline \hline Concrete Edge Failure \\ \hline \hline The initial value V_{0Rk,c,fi} of the characteristic resistance in concrete C20/25 to C50/60 \\ under fire exposure may be determined by: \\ \hline V_{0Rk,c,fi} = 0,25 \times V_{0Rk,c} (\leq R90) & V_{0Rk,c,fi} = 0,20 \times V_{0Rk,c} (\leq R120) \\ \hline \hline \hline With V_{0Rk,c} initial value of the characteristic resistance in cracked concrete C20/25 under \\ \hline \hline \hline \hline \hline \ \ \ \ \ \ \ \ \ \ \ \ \ \$	R30	M <sup>0</sup> <sub>Rk,s,fi</sub>	(kN)	0,21		
R90 $M^0_{Rk,s,fi}$ (kN)0,14R120 $M^0_{Rk,s,fi}$ (kN)0,10Pryout FailureR30 $V_{Rk,cp,fi}$ (kN)R60 $V_{Rk,cp,fi}$ (kN)R90 $V_{Rk,cp,fi}$ (kN)R120 $V_{Rk,cp,fi}$ (kN)R120 $V_{Rk,cp,fi}$ (kN)Oncrete Edge Failure0,33The initial value Vork,c,fi of the characteristic resistance in concrete C20/25 to C50/60 under fire exposure may be determined by:Vork,c,fi = 0,25 x Vork,c (< R90)	R60	M <sup>0</sup> <sub>Rk,s,fi</sub>	(kN)	0,19		
Pryout FailureR30 $V_{Rk,cp,fi}$ (kN)R60 $V_{Rk,cp,fi}$ (kN)R90 $V_{Rk,cp,fi}$ (kN)R120 $V_{Rk,cp,fi}$ (kN)0,330,33Concrete Edge FailureThe initial value Vork,c,fi of the characteristic resistance in concrete C20/25 to C50/60under fire exposure may be determined by:Vork,c,fi = 0,25 x Vork,c (≤ R90)Vork,c,fi = 0,20 x Vork,c (≤ R120)With Vork,c initial value of the characteristic resistance in cracked concrete C20/25 under	R90		(kN)			
$\begin{tabular}{ c c c c c }\hline R30 & V_{Rk,cp,fi} & (kN) & & & & & & & & & & & & & & & & & & &$	R120	M <sup>0</sup> <sub>Rk,s,fi</sub>	(kN)	0,10		
R60V_{Rk,cp,fi}(kN)0,41R90V_{Rk,cp,fi}(kN)R120V_{Rk,cp,fi}(kN)R120V_{Rk,cp,fi}(kN)0,33Concrete Edge FailureThe initial value Vork,c,fi of the characteristic resistance in concrete C20/25 to C50/60 under fire exposure may be determined by:Vork,c,fi = 0,25 x Vork,c (≤ R90)Vork,c,fi = 0,20 x Vork,c (≤ R120)With Vork,c initial value of the characteristic resistance in cracked concrete C20/25 under	Pryout Fa	ilure				
$\begin{tabular}{ c c c c c c c c c c c c c c c c c c c$	R30	V <sub>Rk,cp,fi</sub>	(kN)			
R120       V <sub>Rk,cp,fi</sub> (kN)       0,33         Concrete Edge Failure         The initial value Vork,c,fi of the characteristic resistance in concrete C20/25 to C50/60 under fire exposure may be determined by:         Vork,c,fi = 0,25 x Vork,c (≤ R90)         Vork,c,fi = 0,20 x Vork,c (≤ R120)         With Vork,c initial value of the characteristic resistance in cracked concrete C20/25 under	R60	V <sub>Rk,cp,fi</sub>	(kN)	0,41		
Concrete Edge Failure         The initial value VORK,c,fi of the characteristic resistance in concrete C20/25 to C50/60 under fire exposure may be determined by:         VORK,c,fi = 0,25 x VORK,c (≤ R90)         VORK,c,fi = 0,25 x VORK,c (≤ R90)         With VORK,c initial value of the characteristic resistance in cracked concrete C20/25 under	R90	V <sub>Rk,cp,fi</sub>	(kN)			
Concrete Edge Failure         The initial value VORK,c,fi of the characteristic resistance in concrete C20/25 to C50/60 under fire exposure may be determined by:         VORK,c,fi = 0,25 x VORK,c (≤ R90)         VORK,c,fi = 0,20 x VORK,c (≤ R120)         With VORK,c initial value of the characteristic resistance in cracked concrete C20/25 under	R120	V <sub>Rk,cp,fi</sub>	(kN)	0,33		
With VORK,c initial value of the characteristic resistance in cracked concrete C20/25 under				stance in concrete C20/25 to C50/60		
With VORk,c initial value of the characteristic resistance in cracked concrete C20/25 under	V0Rk,c,fi = 0,25	x V0Rk,c (≤ R90)		V0Rk,c,fi = 0,20 x V0Rk,c (≤ R120)		
			naracteristic resis	tance in cracked concrete C20/25 under		

#### Performances

Fire exposure - characteristic values of shear resistance

of European Technical Assessment

Annex C3

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